



RESEARCH LETTER

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Key Points:

- Variations in pore water pressure cause dramatic changes in friction against ice flow provided by a subglacial sedimentary bed
- When water pressure varies, sediments creep nonlinearly due to force network reorganization at stress levels below the yield strength
- Sediment strength is limited to the Mohr-Coulomb criterion, which can produce stick-slip behavior in systems with stress oscillations

Supporting Information:

- Supporting Information S1
- Figure S1
- Figure S2
- Data Set S1

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Ice flow dynamics forced by water pressure variations in subglacial granular beds

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Abstract Glaciers and ice streams can move by deforming underlying water-saturated sediments, and the nonlinear mechanics of these materials are often invoked as the main reason for initiation, persistence, and shutdown of fast-flowing ice streams. Existing models have failed to fully explain the internal mechanical processes driving transitions from stability to slip. We performed computational experiments that show how rearrangements of load-bearing force chains within the granular sediments drive the mechanical transitions. Cyclic variations in pore water pressure give rise to rate-dependent creeping motion at stress levels below the point of failure, while disruption of the force chain network induces fast rate-independent flow above it. This finding contrasts previous descriptions of subglacial sediment mechanics, which either assume rate dependence regardless of mechanical state or unconditional stability before the sediment yield point. Our new micromechanical computational approach is capable of reproducing important transitions between these two end-member models and can explain multimodal velocity patterns observed in glaciers, landslides, and slow-moving tremor zones.

1. Introduction

Glaciers and ice sheets flow by three main mechanisms [Cuffey and Paterson, 2010]: (1) viscous deformation of ice, (2) sliding at the ice bed interface, and (3) deformation of subglacial sediments [Iverson *et al.*, 1995; Hooke *et al.*, 1997; Tulaczyk *et al.*, 2000]. Fast flow occurs where the ice base is at the pressure melting point, which is governed by the weight of the overlying ice, heat dissipation accompanying sliding and deformation, latent heat, and geothermal flux. Such thermal conditions allow liquid water in the subglacial environment. Hence, sedimentary subglacial beds often host melt water saturated and actively deforming granular materials (till), consisting of either reworked older sedimentary deposits or mobilized products from glacial erosion [Cuffey and Paterson, 2010; Stokes *et al.*, 2016]. Till may become weaker than glacier ice when water pressure is high, because the frictional failure strength of sediments is controlled by effective stress (i.e., the difference between total load and pore water pressure). Till deformation may be the main driver of glacier flow under these conditions [Hooke *et al.*, 1997; Cuffey and Paterson, 2010], and fast ice flow is often collocated with sedimentary beds [Anandkrishnan *et al.*, 1998; Tulaczyk *et al.*, 2000; Peters *et al.*, 2006].

The mechanical behavior of subglacial till is thus of primary importance to the motion of glaciers and ice sheets. However, the grain-scale controls on till strength and deformation style are poorly known. The subglacial environment is difficult to access and experimentally analyze, and the physics of subglacial till deformation has consequently been a topic of long-lasting and intense discussion [e.g., Alley *et al.*, 1986; Boulton and Hindmarsh, 1987; Kamb, 1991; Iverson *et al.*, 1995; Hooke *et al.*, 1997; Iverson *et al.*, 1998; Tulaczyk *et al.*, 2000; Fowler, 2003; Rathbun *et al.*, 2008; Damsgaard *et al.*, 2013, 2015]. The constitutive relations proposed for till range from nearly linear viscous [Alley *et al.*, 1986; Boulton and Hindmarsh, 1987; Alley *et al.*, 1987] to frictional with slight velocity strengthening [Hooke *et al.*, 1997; Kamb, 1991; Tulaczyk *et al.*, 2000; Tulaczyk, 2006] or weakening [Iverson *et al.*, 1998; Iverson and Zoet, 2015]. A nearly linear viscous till would strongly dampen variations in ice flow velocity by increasing or decreasing basal resistance when ice motion accelerates or decelerates, respectively. Models based on plasticity and friction, on the other hand, predict till strength with little or no velocity dependence, and they can explain rapid flow oscillations and unstable feedbacks in glacier flow, which may ultimately lead to ice sheet reorganization or collapse [Kamb, 1991; Parizek *et al.*, 2013; Bougamont *et al.*, 2015; Ritz *et al.*, 2015]. Evidence from in situ measurements and laboratory

experiments strongly supports the latter type of models with little correlation between glacier sliding velocity and subglacial till strength. The strength seems instead to be controlled by effective stress, the fraction of ice overburden that is not carried by subglacial water pressure [Hooke *et al.*, 1997; Fischer and Clarke, 1997; Kamb, 1991; Iverson *et al.*, 1998; Tulaczyk *et al.*, 2000; Damsgaard *et al.*, 2013, 2015].

The influence of effective stress on glacier flow over sedimentary and bedrock beds is supported by several studies showing a positive correlation between surface melt production, subglacial water pressure, and glacier velocity [e.g., Hooke *et al.*, 1997; Fischer and Clarke, 1997; Bartholomaus *et al.*, 2008; Andrews *et al.*, 2014]. Glaciers can accelerate when melt water produced at the surface is routed to the glacier bed, causing water pressure to increase. Likewise, many West Antarctic ice streams that drain ice to the ocean flow at highly variable speeds, because tidal movements in the floating part of the glacier modulate the upstream distribution of pore water pressure and stress from the ice [e.g., Bindshadler *et al.*, 2003; Winberry *et al.*, 2011; Walker *et al.*, 2013; Thompson *et al.*, 2014; Rosier *et al.*, 2015]. Although surface-melting glaciers and Antarctic tidal ice streams are dissimilar in many ways, the basic reason for their variable velocity may be similar: reduction of effective stress weakens the frictional strength of the glacier bed. The impact of effective stress on steady state till rheology has been previously considered [Kamb, 1991; Hooke *et al.*, 1997; Fischer and Clarke, 1997; Iverson *et al.*, 1998; Tulaczyk *et al.*, 2000; Iverson and Iverson, 2001; Damsgaard *et al.*, 2013, 2015] but not the impact of water pressure fluctuations on micromechanical granular stability before and during plastic failure.

2. Methods

In order to study the mechanical response of a granular bed to transient stress perturbations, we designed computational experiments where the force balance of a fluid-saturated granular material is disturbed by variations in effective stress normal to the granular bed (Figure 1). The grains and fluid are simulated using two separate but coupled numerical algorithms, implemented for GPU computing [NVIDIA, 2015]. The granular phase is approximated by the soft-body discrete element method with elastic frictional contacts [Cundall and Strack, 1979; Hinrichsen and Wolf, 2004; Luding, 2008; Kruggel-Emden *et al.*, 2008; Radjai and Dubois, 2011; Damsgaard *et al.*, 2013] and is fully two-way coupled to the fluid phase with water pressures evolving according to changes in porosity and Darcian porous flow [McNamara *et al.*, 2000; Zhou *et al.*, 2010; Goren *et al.*, 2010, 2011; Damsgaard *et al.*, 2015]. The local hydraulic permeability is scaled by local porosity [Hazen, 1910; Kozeny, 1927; Carman, 1937; Harleman *et al.*, 1963; McNamara *et al.*, 2000; Goren *et al.*, 2011; Damsgaard *et al.*, 2015]. The computational experiment involves a small three-dimensional sample ($0.52 \times 0.26 \times 0.55$ m) of sediment represented by 9600 spherical grains of uniform size. The lower boundary is static and impermeable, while a flat and mobile upper wall exerts a defined and time variable normal stress downward onto the granular assemblage. Fluid pressure is adjusted accordingly in the cells containing the upper wall. Fluid mass is conserved everywhere in the domain, with the exception of the uppermost cells with a prescribed water pressure, similar to “drained” geotechnical laboratory setups [e.g., Bowles, 1992]. Lateral boundaries are periodic for both the granular and fluid phases. Prior to the shear experiment, the grains are consolidated under uniaxial compression. A constant shear stress applied to the uppermost layer of grains induces shear movement. Simulation parameters are listed in Table S1 in the supporting information. An extended description of methods is available in Text S1 and references therein. The comparability between experiment and true subglacial setting thus relies on the scale independency of granular geotechnical properties [Fowler, 2003; Tulaczyk, 2006], and the fundamental consistency of the Mohr-Coulomb failure envelope across different materials and grain sizes. The model is not designed to reproduce the ductile behavior of very clay-rich materials.

This approach is new for a subglacial setting but highly rewarding compared to standard continuum methods (i.e., the viscous and plastic models mentioned above), because it obviates a priori assumptions regarding the macroscopic rate dependency of the material strength. Generally speaking, the mechanical behavior of a granular material results from the properties of the individual grains and their collective self-organizing arrangement. Transitions in the mechanical state of granular materials are known to drastically influence the load-bearing capacity [e.g., Jaeger and Nagel, 1992].

The external forcings, namely, shear stress and pore water pressure, were calibrated to mimic subglacial conditions where water pressure may vary at considerably shorter time scales than shear stress. The shear stress was thus held constant at 10 kPa, while pore water pressure at the top of the bed was prescribed to oscillate

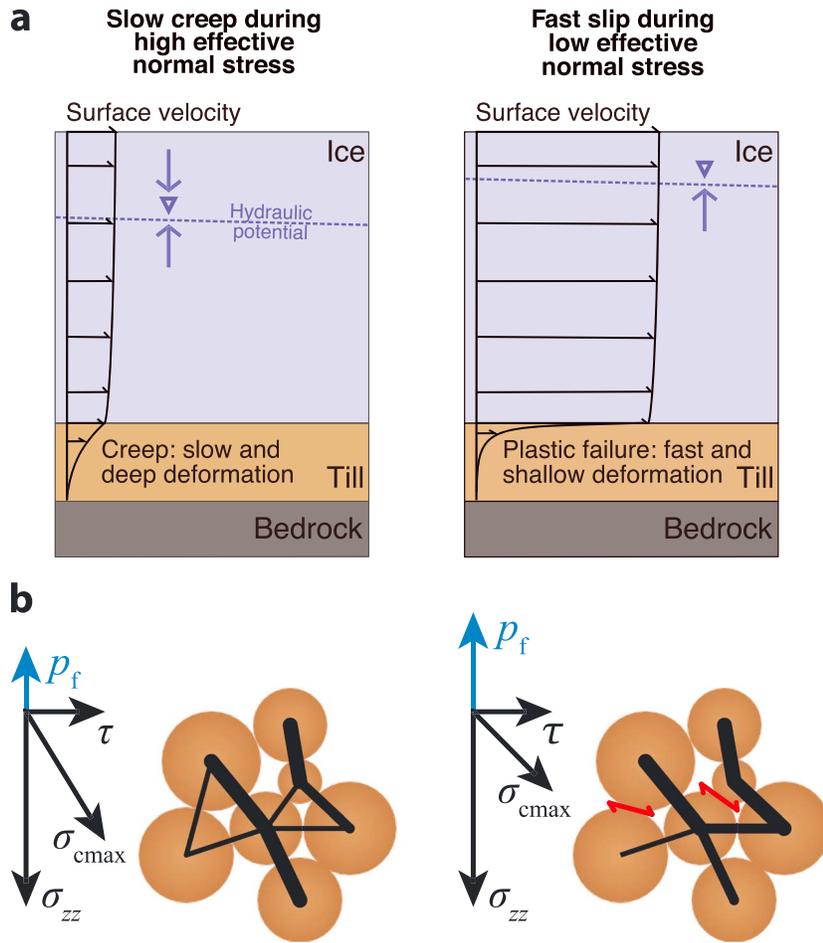


Figure 1. Schematic representation of ice flow and granular deformation in the glacier bed. (a) The granular till bed (left) slowly creeps due to variations in pore water pressure or (right) slips rapidly due to yield failure. Figure is not to scale. (b) Variations in pore water pressure (p_f) modify the direction and magnitude of the maximum compressive strength (σ_{cmax}) in the sedimentary bed. The black lines represent the granular stress and the red arrows denote contact sliding. At lower p_f (left diagram in Figure 1b) grain contact friction inhibits deformation. At higher p_f (right diagram in Figure 1b) grains can slide past each other as internal stresses change over time. The cumulative deformation contributed by grain-scale slip events leads to local reorganization of the granular force network and creeping motion beneath the yield stress and unconstrained bed acceleration at greater driving stresses.

with a diurnal amplitude of 70 kPa, causing changes in effective normal stress around a mean value of 80 kPa (Figure 2a). Plastic failure is known to occur in this simulated material when the magnitude of applied shear stress equals 30% of the effective normal stress or more [Damsgaard *et al.*, 2013, 2015]. All parts of the granular assemblage were free to move and accelerate at any rate dictated by the net force and torque on each grain.

3. Stick, Creep, and Slip

In our experiments, the granular bed showed highly nonlinear velocity variations in response to the fluctuating effective pressure. Periods of minimum motion—stick events, when static force chains caused jamming and a solid-like rigidity of the granular assemblage—were possible during times of maximum effective normal stress and low variation in pore water pressure. In contrast, periods of slip, with rapid deformation of a thin boundary layer of grains, occurred when effective normal stress was lowered enough to push the macroscopic yield strength below the externally imposed shear stress. Moreover, a key finding of our experiments was that the granular material showed creep in the periods between the stick-slip phases with velocities between 10^{-8} and 10^{-6} m/s (Figure 2b and Figure S1 in the supporting information). The rate of creep

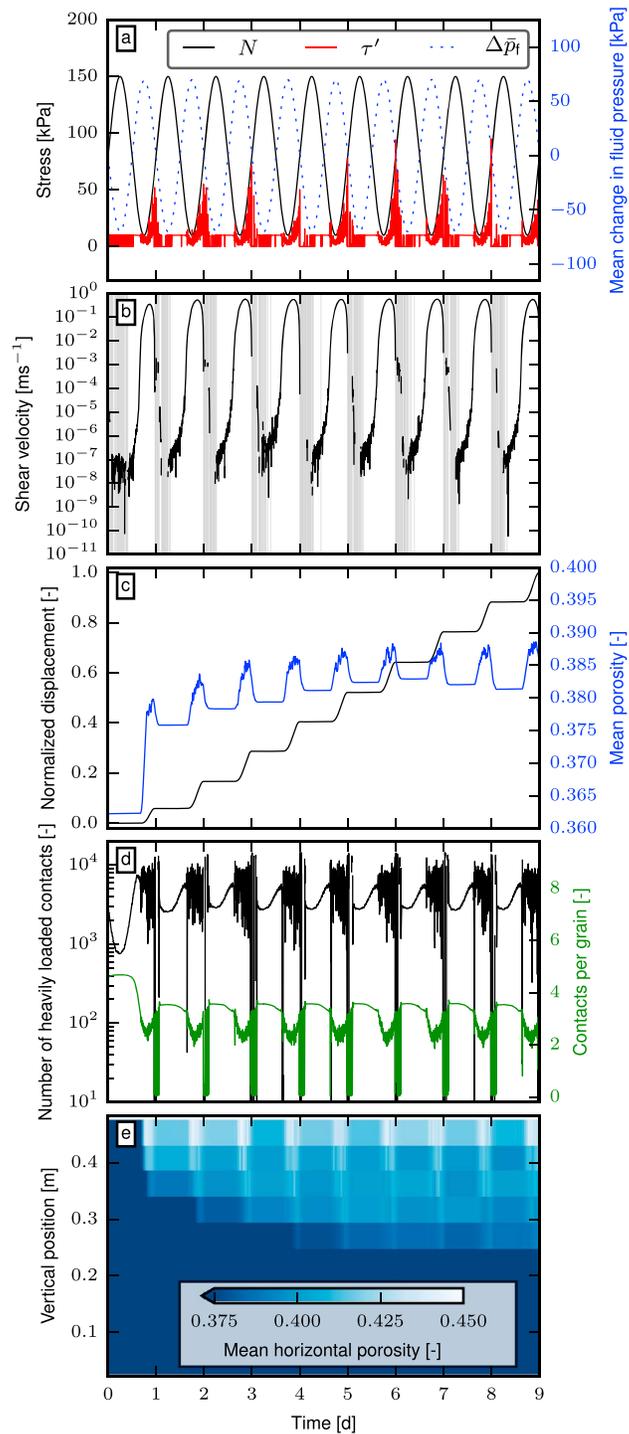


Figure 2. Granular dynamics in computational experiments forced by cyclic variation of water pressure. (a) Cyclic modulation of pore water pressure (Δp_f , blue, right axis) at the upper boundary affects effective normal stress (N ; black, left axis) and changes the ratio between shear stress (τ' ; red, left axis) and the effective normal stress (N). The large values of recorded shear stress occur when the material slows down after runaway failure. (b) The stability of the granular assemblage is determined by the τ'/N ratio, and the material responds by (1) stick during low and decreasing τ'/N ratios (gray vertical bars), (2) slow creep for low and increasing τ'/N ratios, or (3) slip during high τ'/N ratios. (c) The irregular velocity pattern results in a stepwise displacement, where mean porosities are constant during creep and elevated during fast slip. (d) The number of relatively heavily loaded grain pairs increases as the effective normal stress decreases, while the mean number of contacts per particle decreases. (e) The internal porosity increases in areas of active deformation, which become deeper over the course of several cycles.

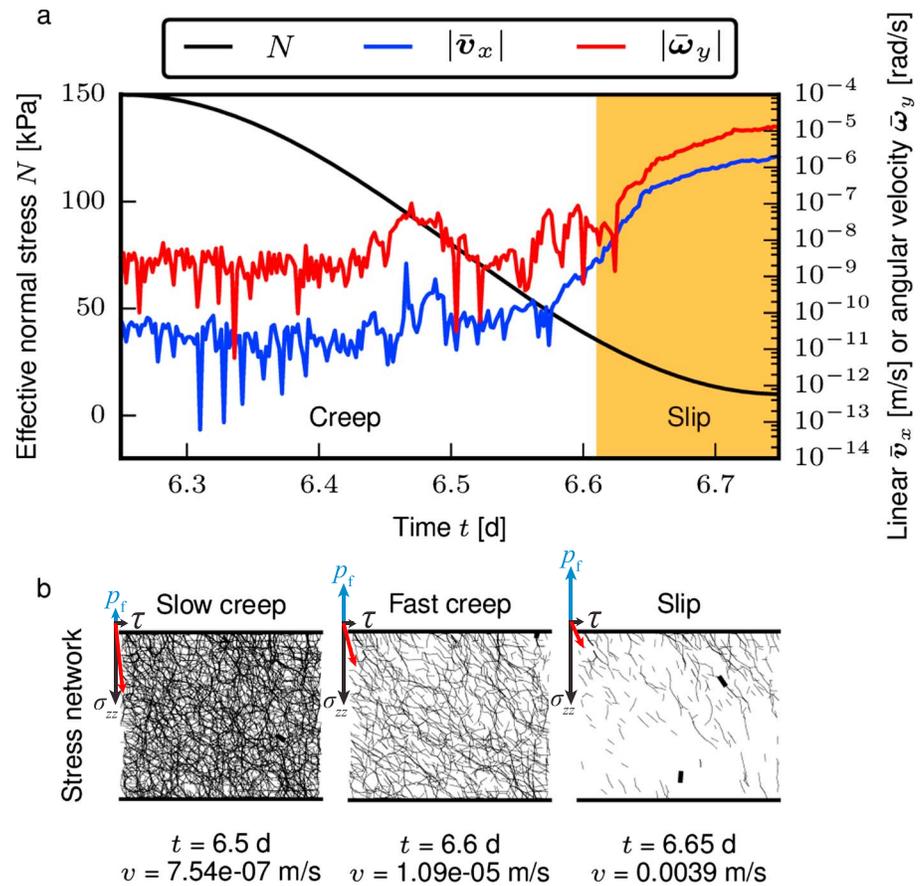


Figure 3. Granular dynamics in response to decreasing effective normal stress. (a) Effective normal stress (black) and averaged grain movement (linear: blue; angular: red). Grain rearrangement accelerates nonlinearly as effective normal stress decreases. The shear velocity contributed by grain rolling is less than the grain linear displacement when converting angular velocity to grain surface displacement rate. (b) Internal distribution of stress between grains (black lines) at different stages of the granular flow. The granular contact stress is mainly in the direction of the applied principal stress represented by the red arrow.

decayed rapidly under constant-stress forcing, but repeated variations in effective normal stress caused the orientation and magnitude of the maximum compressive stress to change correspondingly. These changes required the grains to geometrically reorganize in order to obtain a packing capable of supporting the new orientation of the principal stress (Figure 1b). The grains responded by small-scale deformation by inter-grain contact sliding and reorientation when the contacts were unfavorably oriented relative to the principal stress. The contact reorganization caused relatively large creep velocities and a high level of porosity in the sediment, and the material did not consolidate to prefailure packing under maximum effective normal stress (Figures 2c and 2e). The creep was caused by distributed deformation contrary to the shallow deformation during slip failure.

The finding of prefailure creep in idealized granular materials contrasts with the perfectly plastic material rheology, where no deformation occurs at stress levels below the yield strength. The combination of creep and stick-slip results in a stepped displacement history (Figure 2c). Creep has for a long time been recognized as a deformation mode preceding plastic failure [e.g., Griggs, 1936; Terzaghi, 1950], but the governing processes are poorly constrained. Creep rates in geotechnical materials subjected to a constant deviatoric stress just below its ultimate failure strength are known to decay logarithmically with time [e.g., Kamb, 1991; Moore and Iverson, 2002; Nguyen et al., 2011] or to lead to runaway failure [e.g., Mitchell and Soga, 2006]. Our experiments suggest that repeated perturbation of effective stress causes sustained internal grain rearrangement (Figure 3), which has also recently been observed in laboratory experiments on simple granular materials

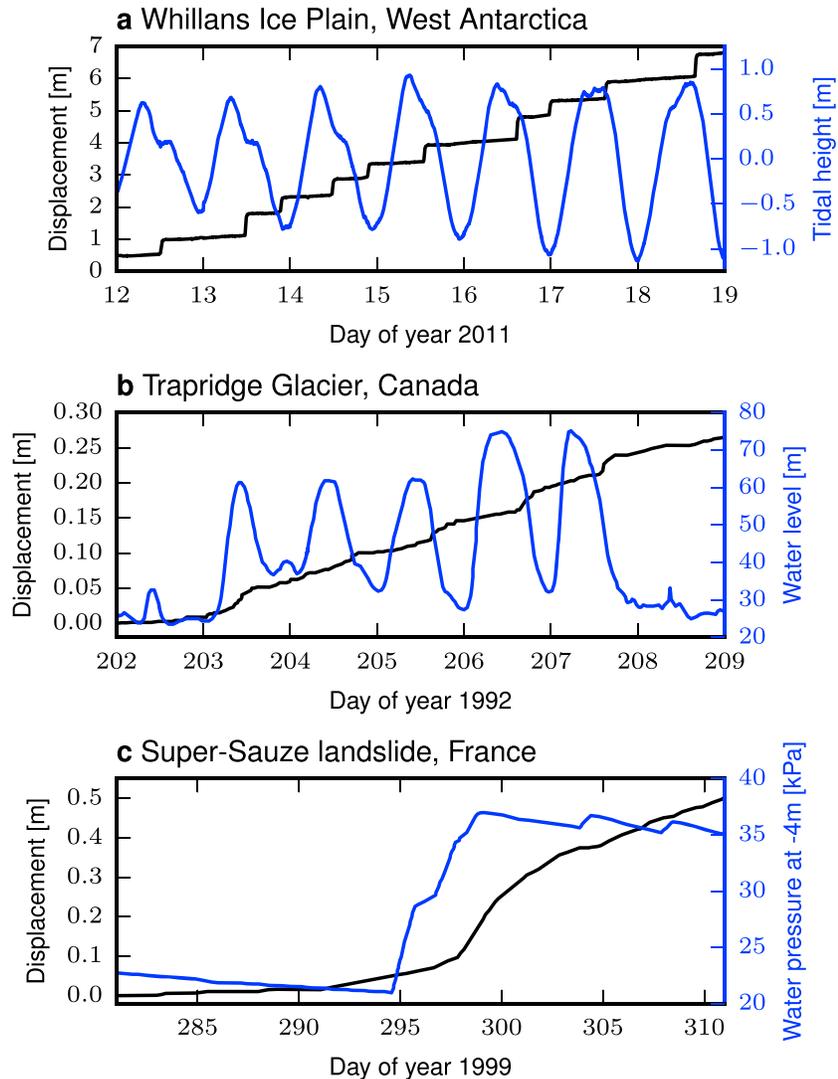


Figure 4. (a, b) Creep and slip due to pore pressure variation in two glacial systems and (c) an active landslide. All three systems display slow but measurable displacement during periods of low but variable water pressure, corresponding to the creep in our numerical simulations (Figure 2b). Trapridge Glacier data from *Fischer and Clarke* [1997], Super-Sauze landslide data from *Malet et al.* [2002].

[*Pons et al.*, 2015]. This behavior is analogous to how granular materials on hillslopes beneath the angle of repose experience downslope movement due to episodic disturbances, e.g., wet-dry or freeze-thaw cycles [*Roering et al.*, 2001]. The flow of slow-moving landslides is sensitive to transient stress perturbations such as variations in pore water pressure by discrete precipitation events [*Roering et al.*, 2001] or variations in atmospheric pressure [*Schulz et al.*, 2009]. Similarly, continued creep is observed in water flow-driven sediment transport [*Houssais et al.*, 2015; *Houssais and Jerolmack*, 2016]. Processes such as fluid migration or the arrival of teleseismic waves can disturb the balance of stresses in earthquake faults and are hypothesized to cause slow-slip tremor episodes or initiate fast slip accompanying earthquakes [*Schwartz and Rokosky*, 2007; *Shelly et al.*, 2011; *Peng et al.*, 2014]. We expect creep to dominate bulk shear strain if the yield strength is not exceeded at all, or if the duration of plastic failure is relatively short. Creep is most significant when the material is stressed just below the yield strength due to the strong observed nonlinearity between driving stresses and the resultant shear strain rate (Figure S1 in the supporting information).

We compared our model results to observations from a mountain glacier, an ice stream, and a landslide, which are all phenomena in which deformation of granular materials plays an important role (Figure 4).

The variations in water pressure have in these settings and in our experiment very different amplitudes. However, from our results we expect that smaller water pressure variations are needed in systems with low effective normal stress, and vice versa. At Whillans Ice Plain, West Antarctica, tidal variations induce flow oscillation (Figures 4a and S2) [Bindschadler *et al.*, 2003; Winberry *et al.*, 2011] and Trapridge Glacier in Canada shows similar displacement when surface melt drains through crevasses to the sedimentary bed, causing periodic ice bed decoupling during drainage and slow movement at low subglacial water pressure (Figure 4b) [Fischer and Clarke, 1997]. The flow of the Super-Sauze landslide in France (Figure 4c) is strongly linked to discrete precipitation events that alter the internal water level [Malet *et al.*, 2002]. In all three settings nonlinear granular dynamics causes flow to switch between fast slip and slow creep. The slip phases correspond to plastic failure of the granular bed when water pressure exceeds a threshold value. Slow flow between slips may be caused by elastic loading, viscoelastic ice deformation, basal sliding in the glacial systems, and the granular creep mechanism presented here. While diurnal-scale variations in pore water pressure drive the granular creep, longer-term changes in mean water pressure set the pace of the creep and influence the duration of slip events [Beem *et al.*, 2014; Winberry *et al.*, 2014; Siegfried *et al.*, 2016]. The creep in our experiments is caused by distributed deformation, while slip is accommodated by shallow deformation. This difference in deformational depth may explain the discrepancy between seismic and in situ investigations of deforming bed thicknesses [e.g., Blankenship *et al.*, 1986; Engelhardt *et al.*, 1990].

4. Summary

Shear deformation of subglacial sediments contributes significantly to ice stream flow in many cases. On diurnal time scales, variations in subglacial water pressure and driving stress can cause stick-slip movement [e.g., Rosier *et al.*, 2015], while on time scales of centuries, the same variations can cause ice stream shutdown and initiation [e.g., Bougamont *et al.*, 2015]. From two-phase computational experiments we demonstrated that stick due to granular jamming is rare, as changes in the deviatoric stress cause grain contact failures leading to prefailure creep that can be fitted with a nonlinear rate-dependent relationship. Above the yield strength the rheology becomes rate independent. Creep will dominate the bulk shear strain if the yield strength is not exceeded, if the duration of plastic failure is short, and/or if driving stresses are close to the yield strength. The extreme sensitivity of granular flow to changes in shear stress or water pressure highlights the importance of understanding the coupled mechanics of stick-slip and creep in a wide range of natural environments. Our micromechanical computational approach offers a solution to explain the observed multimodal velocity patterns in fast moving ice streams, landslides, and tectonic faults by a combination of stick-slip and creep in granular materials.

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